

# Viscous Flow and Heat Transfer Over a Permeable Shrinking Sheet with Partial Slip

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*The viscous flow over a shrinking permeable sheet with partial slip is investigated. The flow is governed by a third-order nonlinear differential equation and heat transfer by a second-order differential equation. The equations of motion are solved analytically by Optimal Homotopy Perturbation Method (OHPM). This procedure is highly efficient and it controls the convergence of the approximate solutions. A few examples are presented, showing the exceptionally good agreement between the analytical and numerical solutions. OHPM is very efficient in practice, ensuring a very rapid convergence after only one iteration.*

*Keywords: Optimal homotopy perturbation method, viscous flow, partial slip, shrinking sheet, heat transfer.*

The flow to a shrinking boundary with partial slip has yet become relevant in many situations and is very significant because of its several applications in engineering or industrial processes for example: glass fiber, crystal growing, paper production, drawing of electric films. Also, there are some situations where there may be a partial slip between the fluid and the boundary, e.g., the fluid may be a rarefied gas as mentioned by Sharipov and Seleznev [1]. The no slip condition is replaced by Navier's partial slip condition, where the amount of relative slip is proportional to the local shear stress. The effect of stagnation slip flow on the heat transfer from a moving plate was recently considered by Wang [2]. Fang et al. [3] have solved the problem of viscous fluid flow model, without considering the heat transfer aspects, and they presented an exact solution of the governing Navier-Stokes equations. A very specific unsteady shrinking film solution was discussed by Wang [4]. The properties of the flow due to a shrinking sheet with suction are studied by Miklavčič and Wang [5]. Suction occurs when the fluid condenses on the surface, such as in chemical vapour deposition is considered by Jensen et al. [6]. The boundary layer flow and heat transfer over a permeable shrinking sheet with a first order slip flow model and the heat transfer rate at the surface are investigated by Aman and Ishak [7].

The objective of the present paper is to propose an accurate approach to nonlinear differential equation of a viscous fluid over a shrinking permeable sheet with partial slip and the heat transfer at the surface, using an analytical technique, namely optimal homotopy perturbation method [8-11]. The validity of our procedure, which does not imply the presence of a small or large parameter in the equation or into the boundary / initial conditions is based on the construction and determination of the auxiliary functions, combined with a convenient way to optimally control the convergence of the solution. The efficiency of our procedure is proved while an accurate solution is explicitly analytically obtained in an iterative way after only one iteration. The validity of this method is determined by comparing the results obtained with the results given by the numerical integration.

## Equation of motion

Consider a two-dimensional laminar boundary layer flow over a shrinking boundary. If  $(u, v)$  is the velocity components in the Cartesian directions  $(x, y)$  and  $T$  is the temperature in the boundary layer, then the boundary layer equations are

$$u_x + v_y = 0 \quad (1)$$

$$uu_x + vu_y = \nu u_{yy} \quad (2)$$

$$uT_x + vT_y = \alpha T_{yy} \quad (3)$$

where  $\nu$  is the kinematic viscosity and  $\alpha$  is the thermal diffusivity.

The partial slip boundary conditions are:

$$\begin{aligned} u = -ax + kvu_y, \quad v = V_w, \quad T = T_w, \quad \text{at } y = 0 \\ u \rightarrow 0, \quad T \rightarrow T_\infty \quad \text{as } y \rightarrow \infty \end{aligned} \quad (4)$$

where  $a > 0$  is the shrinking constant,  $k$  is a constant of proportionality,  $V_w$  is the mass transfer velocity at the surface of the sheet with  $V_w > 0$  for injection,  $V_w < 0$  for suction and  $V_w = 0$  for impermeable sheet,  $T_w$  is constant surface temperature.

In order to simplify the governing equations we use the similarity transformations:

$$\eta = \left(\frac{a}{\nu}\right)^{1/2} y, \quad \psi = (av)^{1/2} xF(\eta), \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty} \quad (5)$$

where  $\eta$  is the independent similarity variable,  $F(\eta)$  is the dimensionless stream function,  $\theta(\eta)$  is the dimensionless temperature and  $\psi$  is the stream function defined as  $u = \psi_y$  and  $v = -\psi_x$  such that eq. (1) is automatically satisfied. From eq. (5) we get

$$u = axF'(\eta), \quad v = -(av)^{1/2} F(\eta) \quad (6)$$

where prime denotes differentiation with respect to  $\eta$ .

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If we note  $s = F(0)$ , then we take

$$V_w = -(av)^{1/2} s \quad (7)$$

Eqs (2) and (3) are reduced to the ordinary differential equations:

$$F'''(\eta) + F(\eta)F''(\eta) - [F'(\eta)]^2 = 0 \quad (8)$$

$$\theta''(\eta) + Pr F(\eta)\theta'(\eta) = 0 \quad (9)$$

where  $Pr = \nu / \alpha$  is the Prandtl number.

Now, the boundary conditions (4) can be written in the form

$$F(0) = s, \quad F'(0) + l = \lambda F''(0), \quad F'(\eta) \rightarrow 0 \quad \text{as } \eta \rightarrow \infty \quad (10)$$

$$\theta(0) = 1, \quad \theta(\eta) \rightarrow 0 \quad \text{as } \eta \rightarrow \infty \quad (11)$$

where  $\lambda = k \sqrt{av}$  is a nondimensional parameter indicating the relative importance of partial slip. If  $\lambda = 0$  there is no slip and if  $\lambda \rightarrow \infty$ , the surface is stress free [7].

### Basic ideas of optimal homotopy perturbation method

We consider the following nonlinear differential equation

$$L(u) + N(u) = 0 \quad (12)$$

subject to the initial / boundary conditions

$$B\left(u, \frac{\partial u}{\partial \eta}\right) = 0 \quad (13)$$

where  $L$  is a linear operator,  $N$  is a nonlinear operator and  $B$  is a boundary operator.

Generally speaking, the nonlinear operator  $N(u)$  depends on  $\eta, u, u', u''$  and  $u'''$  and therefore one can write:

$$N(u) = G(\eta, u, u', u'', u''') \quad (14)$$

Applying the Taylor series theorem for real values  $\alpha, \beta, \gamma, \delta$ , we obtain

$$\begin{aligned} G(\eta, u + \alpha, u' + \beta, u'' + \gamma, u''' + \delta) = \\ = G(\eta, u, u', u'', u''') + \frac{\alpha}{1!} G_u(\eta, u, u', u'', u''') + \\ + \frac{\beta}{1!} G_{u'}(\eta, u, u', u'', u''') + \frac{\gamma}{1!} G_{u''}(\eta, u, u', u'', u''') + \dots \end{aligned} \quad (15)$$

We consider a homotopy, introducing a number of unknown auxiliary functions  $K_{ij}(\eta, C_k)$ ,  $i, j, k = 1, 2, \dots$  that depend on the variable  $\eta$  and some parameters  $C_1, C_2, \dots$  which satisfies the following equation [8]:

$$\begin{aligned} H(u, p) = L(u) + p[K_{11}(\eta, C_k)G(\eta, u_0, u_0', u_0'', u_0''') + \\ + K_{12}(\eta, C_k)G_u(\eta, u_0, u_0', u_0'', u_0''') + K_{13}(\eta, C_k)G_{u'}(\eta, u_0, u_0', u_0'', u_0''') + \\ + K_{14}(\eta, C_k)G_{u''}(\eta, u_0, u_0', u_0'', u_0''')] \end{aligned} \quad (16)$$

where  $p \in [0, 1]$  is an embedding parameter,  $u_0$  is an initial guess of the solution  $u(\eta, C_k)$  which satisfies the boundary conditions:

$$L(u_0) = 0, \quad B\left(u_0, \frac{\partial u_0}{\partial \eta}\right) = 0 \quad (17)$$

So, it is quite right to assume that the solutions of eq. (16) can be expressed as

$$u = u_0 + pu_1 + p^2u_2 + \dots \quad (18)$$

The first-order approximate solutions of eq. (12) can be readily obtained

$$\bar{u}(\eta, C_k) = u_0(\eta) + u_1(\eta, C_k) \quad (19)$$

where  $u_1(\eta, C_k)$  is obtained by equating the coefficient of  $p$  for eq. (16). More precisely we have the following equation for  $u_1$ :

$$\begin{aligned} L(u_1) + K_{11}(\eta, C_k)G(\eta, u_0, u_0', u_0'', u_0''') + \\ + K_{12}(\eta, C_k)G_u(\eta, u_0, u_0', u_0'', u_0''') + K_{13}(\eta, C_k)G_{u'}(\eta, u_0, u_0', u_0'', u_0''') + \\ + K_{14}(\eta, C_k)G_{u''}(\eta, u_0, u_0', u_0'', u_0'''), \quad B\left(u_1, \frac{\partial u_1}{\partial \eta}\right) = 0 \end{aligned} \quad (20)$$

In our procedure we can write only two equations: (17) and (20). The auxiliary functions  $K_{ij}$ ,  $i = 1, 2, \dots, 5$  are not unique and they can be chosen so that the products  $K_{ij}G_a$  and  $G_a$  to be of the same form ( $a = u, u', u''$  or  $u'''$ ). The convergence-control parameters  $C_k$ ,  $k = 1, 2, \dots$ , which appear in the expression of the functions  $K_{ij}(\eta, C_k)$  can be optimally determined. This can be done via various methods such as: the least squares method, the weighted residual, the collocation method, the Galerkin method and so on. The solutions of eqs. (12) and (13) can immediately be determined once the convergence-control  $C_k$  are known.

### Application of OHPM to viscous flow and heat transfer given by eqs. (8-11)

We apply our procedure to obtain approximate solutions of eqs. (12) and (13). We choose the linear operator  $L$  by the form

$$L(F(\eta)) = F'''(\eta) + KF''(\eta) \quad (21)$$

where  $K > 0$  is an unknown parameter.

Equation (17) becomes

$$\begin{aligned} F_0'''(\eta) + KF_0''(\eta) = 0, \\ F_0(0) = s, \quad F_0'(0) + l = F_0''(0), \quad F_0'(\infty) = 0 \end{aligned} \quad (22)$$

which has the following solution

$$F_0(\eta) = s + \frac{e^{-K\eta} - 1}{K(1 + \lambda K)} \quad (23)$$

The nonlinear operator is given from eqs (12), (8) and (21):

$$N(F(\eta)) = F(\eta)F''(\eta) - KF''(\eta) - [F'(\eta)]^2 \quad (= G(F, F', F'')) \quad (24)$$

From eq. (24) we obtain

$$\begin{aligned} G_F(F, F', F'') = F''(\eta); \quad G_{F'}(F, F', F'') = \\ = -2F'(\eta); \quad G_{F''}(F, F', F'') = F(\eta) - K \end{aligned} \quad (25)$$

Substituting eq. (23) into eqs (24) and (25) we have

$$\begin{aligned} G(F_0) = \frac{\lambda s K^2 - \lambda K^3 + sK - K^2 - 1}{1 + \lambda K} e^{-K\eta}; \quad G_F(F_0) = \frac{K}{1 + \lambda K} e^{-K\eta}; \\ G_{F'}(F_0) = \frac{2}{1 + \lambda K} e^{-K\eta}; \quad G_{F''}(F_0) = s - K + \frac{e^{-K\eta} - 1}{K(1 + \lambda K)} \end{aligned} \quad (26)$$

Equation (20) can be written in the form

$$F_1'''+KF_1''+K_{11}(\eta, C_k) \frac{\lambda sK^2 - \lambda K^3 + sK - K^2 - 1}{1 + \lambda K} e^{-K\eta} + K_{12}(\eta, C_k) \frac{K}{1 + \lambda K} e^{-K\eta} + K_{13}(\eta, C_k) \frac{2}{1 + \lambda K} e^{-K\eta} + K_{14}(\eta, C_k) \left[ s - K - \frac{1}{K(1 + \lambda K)} + \frac{e^{-K\eta}}{K(1 + \lambda K)} \right] = 0, \quad (27)$$

$$F_1(0) = 0, \quad F_1'(0) = \lambda F_1''(0), \quad F_1'(\infty) = 0$$

Having in view eq. (27), the auxiliary functions  $K_{ii}(\eta, C_k)$ ,  $i = 1, 2, 3, 4$ , must follow the terms in this equation, such that we can choose the functions  $K_{ii}(\eta, C_k)$  in the following form:

$$K_{11} = K_{12} = K_{13} = 0, \quad K_{14} = -(1 + \lambda K) \left[ (C_1 + C_2\eta)e^{-K\eta} + (C_3 + C_4\eta)e^{-2K\eta} + (C_5 + C_6\eta)e^{-3K\eta} \right] \quad (28)$$

where  $C_j$ ,  $j = 1, 2, \dots, 6$ , are unknown parameters at this moment.

Substituting eq. (28) into eq (27), we obtain equation in  $F_1(\eta)$

$$F_1'''+KF_1'' = (AC_1 + AC_2\eta)e^{-K\eta} + [C_1 + AC_3 + (C_2 + AC_4)\eta]e^{-2K\eta} + [C_3 + AC_5 + (C_4 + AC_6)\eta]e^{-3K\eta} + (C_5 + C_6\eta)e^{-4K\eta}, \quad (29)$$

where  $A = \lambda sK^2 - \lambda K^3 + sK - K^2 - 1$

Now, solving eq. (29) and then substituting this result and eq. (23) into eq. (19), we obtain the approximate solution of the first-order in the form:

$$\bar{F}(\eta, C_1, C_2, C_3, C_4, C_5, C_6) = s + \alpha - \frac{1}{K(1 + \lambda K)} + \left[ \frac{AC_2}{2K^2}\eta^2 + \left( \frac{2AC_2}{K^3} + \frac{AC_1}{K^2} \right)\eta + \beta + \frac{1}{K(1 + \lambda K)} \right] e^{-K\eta} - \left( \frac{C_2 + AC_4}{4K^3}\eta + \frac{C_2 + AC_4}{2K^4} + \frac{C_1 + AC_3}{4K^3} \right) e^{-2K\eta} - \left( \frac{C_4 + AC_6}{18K^3}\eta + \frac{7C_4 + 7AC_6}{108K^4} + \frac{C_3 + AC_5}{18K^3} \right) e^{-3K\eta} - \left( \frac{C_6}{48K^3}\eta + \frac{5C_6}{288K^4} + \frac{C_5}{48K^3} \right) e^{-4K\eta}, \quad (30)$$

where

$$\alpha = -\frac{1 + 3\lambda K + 8\lambda KA + 4A}{4K^3(1 + \lambda K)} C_1 - \frac{1 + 2\lambda K + 12\lambda KA + 8A}{4K^4(1 + \lambda K)} C_2 - \frac{4 + 16\lambda K + 27\lambda KA + 9A}{36K^3(1 + \lambda K)} C_3 - \frac{8 + 20\lambda K + 54\lambda KA + 27A}{108K^4(1 + \lambda K)} C_4 - \frac{9 + 45\lambda K + 64\lambda KA + 16A}{144K^3(1 + \lambda K)} C_5 - \frac{27 + 120\lambda K + 160\lambda KA + 64A}{864K^4(1 + \lambda K)} C_6 \quad (31)$$

$$\beta = \frac{1 + 45\lambda K + 4\lambda KA + 2A}{2K^3(1 + \lambda K)} C_1 + \frac{3 + 4\lambda K + 12\lambda KA + 8A}{4K^4(1 + \lambda K)} C_2 + \frac{1 + 3\lambda K + 6\lambda KA + 3A}{6K^3(1 + \lambda K)} C_3 + \frac{8 + 20\lambda K + 54\lambda KA + 27A}{108K^4(1 + \lambda K)} C_4 - \frac{9 + 45\lambda K + 64\lambda KA + 16A}{144K^3(1 + \lambda K)} C_5 - \frac{27 + 81\lambda K + 160\lambda KA + 64A}{864K^4(1 + \lambda K)} C_6 \quad (32)$$

For eqs. (9) and (11), the linear operator and nonlinear operator are respectively:

$$L(\theta(\eta)) = \theta'' + h\theta', \quad N(\theta(\eta)) = \theta'(Pr F - h) \quad (= G(\eta)) \quad (33)$$

where  $h$  is an unknown parameter.

In this case, eq. (17) becomes

$$\theta_0'' + h\theta_0' = 0, \quad \theta_0(0) = 1, \quad \theta_0(\infty) = 0 \quad (34)$$

and has the solution

$$\theta_0(\eta) = e^{-h\eta} \quad (35)$$

Substituting eq. (35) into nonlinear operator  $G(\theta)$  and  $G_0(\theta)$ , we obtain

$$G(\theta_0) = B_1 e^{-h\eta} + B_2 e^{-(h+\lambda K)\eta}, \quad G_0(\theta_0) = B_3 + B_4 e^{-K\eta} \quad (36)$$

$$B_1 = h^2 - Pr s h + \frac{Pr h}{K(1 + \lambda K)}, \quad B_2 = -\frac{Pr h}{K(1 + \lambda K)}, \quad B_3 = Pr s - h - \frac{Pr}{K(1 + \lambda K)}, \quad B_4 = \frac{Pr}{K(1 + \lambda K)}. \quad (37)$$

Choosing the auxiliary functions  $K_{2i}(\eta, D_k)$  in the form

$$K_{21}(\eta, D_k) = -(D_1 + D_2 h), \quad K_{22}(\eta, D_k) = -(D_3 + D_4 h) e^{-h\eta} \quad (38)$$

where  $D_j$   $j = 1, 2, 3, 4$  are unknown parameters, equation from which we can obtain the first-approximation  $\theta_1$  is given by

$$\theta_1'' + h\theta_1' = (B_1 D_1 + B_1 D_2 \eta) e^{-K\eta} + [B_2 D_1 + B_4 D_3 + (B_2 D_2 + B_4 D_4)\eta] e^{-(K+h)\eta} + (B_3 D_3 + B_3 D_4 h) e^{-h\eta}, \quad \theta_1(0) = \theta_1(\infty) = 0 \quad (39)$$

The first-order approximate solution of eqs (9) and (11) can be obtained from the solution of eq. (39) and from eq. (35) and has the form

$$\begin{aligned} \bar{\theta}(\eta, D_i) = \theta_0 + \theta_1 = & \left[ \gamma + 1 - \left( \frac{B_3 D_3}{h} + \frac{B_3 D_4}{h^2} \right) \eta - \frac{B_3 D_4}{2h} \eta^2 \right] e^{-h\eta} + \\ & + \left[ \frac{(2K-h)B_1 D_2}{K^2(K-h)^2} + \frac{B_1 D_1}{K(K-h)} + \frac{B_1 D_2}{K(K-h)} \eta \right] e^{-K\eta} + \\ & + \left[ \frac{B_2 D_1 + B_4 D_3}{K(K+h)} + \frac{(2K+h)(B_2 D_2 + B_4 D_4)}{K^2(K+h)^2} + \frac{B_2 D_2 + B_4 D_4}{K(K+h)} \eta \right] e^{-(K+h)\eta}, \end{aligned} \quad (40)$$

where

$$\gamma = -\frac{B_1 D_1}{K(K-h)} + \frac{(h-2K)}{K^2(K-h)^2} B_1 D_2 - \frac{B_2 D_1 + B_4 D_3}{K(K+h)} - \frac{(2K+h)(B_2 D_2 + B_4 D_4)}{K^2(K+h)^2}$$

### Numerical examples

We illustrate the accuracy of OHPM by comparing obtained approximate solutions with the numerical integration results obtained by means of a fourth-order Runge-Kutta method in combination with the shooting method. The unknown parameters are optimally identified via the least square method.

**Example 5.1** In the first case, we consider  $s = 3, \lambda = 1, Pr = 0.71$  and therefore eqs (32) and (40) respectively, can be written effectively in the form

$$\begin{aligned} \bar{F}(\eta) = & 2.9122291658 + (0.0670048355 - 0.0291788256 \eta + \\ & + 0.0037570554 \eta^2) e^{-2.2751183999\eta} - (-0.0124569138 - 0.0330768587 \eta) e^{-4.5502367998\eta} - \\ & - (-0.0085355524 - 0.0060134134 \eta) e^{-6.8253551997\eta} - \\ & - (0.0002264677 + 0.0001971281 \eta) e^{-9.1004735996\eta} \end{aligned} \quad (41)$$

$$\begin{aligned} \bar{\theta}(\eta) = & (-2.4170393387 + 0.4046215594 \eta - 0.0107990954 \eta^2) e^{-2.1296349373\eta} + \\ & + (3.4119615848 + 0.1488146412 \eta) e^{-2.2751183999\eta} - \\ & - (0.0050777538 - 0.0095415500 \eta) e^{-4.4047533372\eta} \end{aligned} \quad (42)$$

**Example 5.2** In the last case, for  $s = 2, \lambda = 3, Pr = 11$

$$\begin{aligned} \bar{F}(\eta) = & 0.3073746342 + (3.4774214710 - 0.1378791520 \eta + \\ & + 0.0177220631 \eta^2) e^{-0.3839040237\eta} - (-4.4441933856 + 1.4747157246 \eta) e^{-0.7678080474\eta} - \\ & - (2.5607893726 + 2.2856461327 \eta) e^{-1.1517120711\eta} - \\ & - (3.6682001183 + 0.4569766849 \eta) e^{-1.5356160948\eta} \end{aligned} \quad (43)$$

$$\begin{aligned} \bar{\theta}(\eta) = & (0.0830361216 - 0.0041430597 \eta) e^{-0.3839040237\eta} + \\ & + (-3.3280711666 + 0.8764027609 \eta + 0.1850908125 \eta^2) e^{-1.9244601113\eta} + \\ & + (4.2450350449 + 0.8544423327 \eta) e^{-2.3083641350\eta} \end{aligned} \quad (44)$$

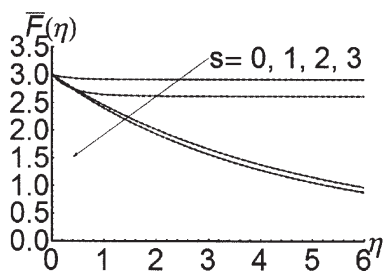


Fig. 1 Variation of  $\bar{F}$  by increasing the partial slip parameter  $\lambda$  and  $s = 3$ :  
 — numerical solution;  
 - - - approximate solution

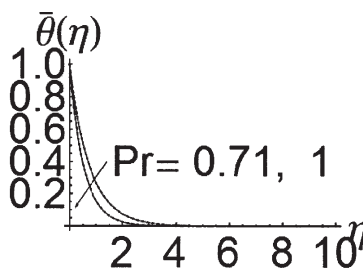


Fig. 2 Temperature profiles  $\bar{\theta}$  for two values of  $Pr$ , and  $s = 2, \lambda = 1$ :  
 — numerical solution;  
 - - - approximate solution;

In figures 1 and 2 are plotted a comparison between the first-order approximate solutions and numerical results obtained by means of the fourth-order Runge-Kutta method in combination with the shooting method.

### Conclusions

In this work, the Optimal Homotopy Perturbation Method (OHPM) is employed to propose an analytic approximate solution to the viscous flow and heat transfer over a permeable shrinking sheet with partial slip parameter. Our procedure is valid even if the nonlinear equation of the motion does not contain any small or large parameters. The proposed approach is mainly based on a new construction of the solutions and especially on the involvement of the convergence-control parameters via the auxiliary functions. These parameters lead to an excellent agreement of the solutions with numerical results. This technique is very effective, explicit and accurate for nonlinear approximations rapidly converging to the exact solutions after only one iteration. The boundary layer equations governing the flow reduced to ordinary differential equations using a similarity transformation. These equations are solved to obtain the displacement and temperature distributions for various values of the partial slip parameter, mass suction parameter and Prandtl number. The effect of partial slip parameter and mass suction parameter, strongly influence the flow displacement and the temperature distribution in the boundary layer.

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